COMPUTATIONAL SIMULATION OF BLAST LOADING IN AN OPEN CYLINDER MODEL USING ANSYS AND LS-DYNA

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(Type 2 Cylinder: Lagrange ConWep)

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INTRODUCTION

- Open cylinder models can be used for testing the materials, which are used in nuclear reactors and containers that are used to store and/or test explosive materials.
- Reduction in the integrity of the cylinder at any stage of transportation or storage can be fatal to the people in the vicinity as well as to the environment.
- Care should be taken to ensure that these cylinders could resist blast-loading during accidents.
- FEA techniques succeed in reducing the time and effort spent in building and testing prototypes.
OBJECTIVE

- FEA is used to simulate the blast-loading in cylinders made of basalt plastic and steel 20 and to validate with the results obtained experimentally.
- The displacement of the cylinder is monitored throughout the simulation and compared to the actual displacement of the cylinder.
- To study the behavior of the candidate structural materials, namely basalt plastic and steel 20 that can be used in nuclear reactors and containers for storing and/or test explosive materials.
- To develop the computational modeling capability to efficiently design cylinder, which can be used for storing and testing explosives.
- To benchmark the ability of ANSYS and LS-DYNA to simulate the blast-loading in the cylinder.
OBJECTIVE (Cont’d.)

- The goal of this project is focused on the determination of the following:
  1. Peak tensile strain in the circumferential direction: $\varepsilon_1$
  2. The time to reach the peak tensile strain in the circumferential direction: $t_1$
  3. Radial oscillation fundamental tone period: $T$
  4. Peak compressive strain in the circumferential direction: $\varepsilon_2$
  5. Peak tensile and compressive strain in the longitudinal direction: $\varepsilon_3$
  6. Peak circumferential strain rate: $d\varepsilon_1/dt_1$
BLAST LOADING TEST

- The blast-loading test in cylinders is performed to investigate the dynamic performance of various candidate structural materials.

- The primary objective is to conduct detailed theoretical and computational studies of the crucial elements of the cylinder.

- The design of the cylinder must ensure complete localization of the detonation products.

- The length of the cylinder is designed to completely contain the blast loading due the explosive that is placed at the center of its’ longitudinal axis.

- This test helps in performing a detailed analysis of stress-strain state of the container and also to determine the explosion resistance of the basalt plastic and steel 20.
The blast loading experiment is simulated computationally using ANSYS and LS-DYNA to analyze the large deformation dynamic response of the cylinder.

Any finite element simulation has three main stages:

- Pre-processing
- Solution
- Post-processing
PRE-PROCESSING : Material Properties

- **Basalt plastic** (EDT - 10 Binder, RB9 - 1200 complex basalt thread roving): Thread diameter = 9 mm; Winding angles: 90° and ±35°

- **Steel 20**: Density = 7850 kg/m³; Yield Strength = 340 MPa; E = 200 GPa, n = 0.33

- **Overall composite properties in the X-Y coordinate system**:
  - The blast loading test in cylinders is performed to investigate the dynamic performance of various candidate structural materials.
  - Fibers are interchanged between q = ±35° and q = 90°
  - $E_x = 15.44$ GPa; $E_y = 48.54$ GPa; $E_z$ (thickness direction) = 14 GPa
  - $G_{xy} = 6.645$ GPa; $G_{yz} = 3$ GPa; $G_{xz} = 3$ GPa
  - $n_{xy} = 0.098$; $n_{xz} = n_{yz} = 0.3$; Density = 2.06 g/cm³
PRE-PROCESSING : Material Geometry

- ANSYS version 7.1 was used to create the geometry of the modeled cylinder.
- Here the modeled cylinder is made of composite material (basalt plastic) having a length of 600 mm and an outer and inner diameter of 321.14 mm and 295 mm, respectively.
- The model also has a liner made of steel 20 of thickness 2.0 mm.
# LINE DIAGRAM OF HOLLOW CYLINDER

![Diagram of Hollow Cylinder](image)

<table>
<thead>
<tr>
<th>Description</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Comp. Thick., $h_1$ [mm]</td>
<td>13.07</td>
</tr>
<tr>
<td>Outer Radius, $R_{out}$ [mm]</td>
<td>160.62</td>
</tr>
<tr>
<td>Steel Thick., $h_2$ [mm]</td>
<td>2.0</td>
</tr>
<tr>
<td>$M_1 + M_2$ [g]</td>
<td>23,700</td>
</tr>
<tr>
<td>$M_{HE}$ [g]</td>
<td>407.3</td>
</tr>
<tr>
<td>Scale factor</td>
<td>1.13</td>
</tr>
</tbody>
</table>
Here, two cases were considered.

- **Case I**: Basalt plastic was considered to be solid while steel was considered as shell
- **Case II**: Both basalt plastic and steel was considered as solid
- **Case I & II:**

  The element types were defined. In case of basalt plastic, the material model chosen was elastic orthotropic whereas for the steel liner, elastic isotropic material model was chosen.

*MAT_ORTHOTROPIC_ELASTIC*

```
1  0.206E+03  0.154E+11  0.485E+11  0.140E+11  0.098000  0.300000  0.300000
  0.664E+10  0.300E+10  0.300E+10  0.0
  0.0  0.0  0.0  0.0  0.0  0.0
  0.0  0.0  0.0  0.0  0.0  0.0  0.0
```

*MAT_ELASTIC*

```
2  0.785E+04  0.200E+12  0.330000  0.0  0.0  0.0
```
• **Case 1**

The real constant set number for thin shell was defined. Then the cylinder was modeled by using cylinder option in create command in modeling module.

• **Case 2**

Since shell was not considered, real constant set number option was not used here and the cylinder was modeled by using cylinder option in create command in modeling module.
PRE-PROCESSING : Meshing

Case 1:

Here the cylinder was meshed in the form of both shell and solid elements. The steel liner was meshed as the shell elements while the basalt plastic was meshed as solid elements. The model had a total of 6000 elements, out of which 1200 are shell elements and 4800 are solid elements.

Case 2:

Here the cylinder was meshed in the form of solid elements only. Both the steel liner and basalt plastic was meshed as solid elements. The model had 6500 solid elements.
Meshed Model of a Cylinder
(Case I: Composite: Solid and Steel: Shell)
Meshed Model of a Cylinder
(Case II: Composite and Steel: Solid)
In order to specify the type and frequency of generating the output files, the following keywords were used:

*DATABASE_BINARY_DEPLOT: This creates a database file, named, “d3plot” that contains the plotting information of the plot data over the three dimensional geometry of the model. Under this option, the user can specify the frequency of the outputs. In other words, one can choose the frequency with which the plot data can be generated. Careful selection of this frequency, depending on the total time of simulation, reduces simulation time.

*DATABASE_BINARY_D3THDT: This generates a database file, named, “d3thdt” that contains time history data of element subsets or global information. Under this option too, the frequency of output can be specified.
The following were the parameters that were specified before running the solution:

- **Case I:** To call the ConWep function, the input deck must contain *
  LOAD SHELL SET* and *
  LOAD BLAST* cards.

- The purpose of *
  LOAD BLAST* card to is define an airblast function for the application of pressure loads due to explosives in conventional weapons. This option determines the pressure values when used in conjunction with the *
  LOAD SHELL SET*.

```
*LOAD SHELL SET
$(Defines which shell to apply *LOAD BLAST)
$------------------------2------------------------3------------------------4------------------------5------------------------6------------------------7------------------------8
$                      SID     LCID      SF      AT
  222                  -2       1       0
*LOAD BLAST
$ WGT XBO YBO ZBO TBO IUNIT ISURF
$------------------------2------------------------3------------------------4------------------------5------------------------6------------------------7------------------------8
  0.4602                0       0       0.3      0      2       2
```
In addition, the following cards were also included in the .k file as follows

```
*SET_SHELL_LIST_GENERATE
$--------1--------2--------3--------4--------5--------6--------7--------8
$    SID   DA1   DA2   DA3   DA4
    222
     1   360
*DEFINE_CURVE
$--------1--------2--------3--------4--------5--------6--------7--------8
   4     0  1.000  1.000  0.000  0.000
0.000000000000E+00  0.000000000000E+00
1.000000000000E+00  0.000000000000E+00
$
$
*DEFINE_CURVE
$--------1--------2--------3--------4--------5--------6--------7--------8
 25     0  1.000  1.000  0.000  0.000
0.000000000000E+00  0.000000000000E+00
1.000000000000E+00  0.000000000000E+00
$
$
```

This input file thus generated was fed to LS-DYNA solver.
Case II: Since, here both materials are considered as solid, it is necessary to identify nodes and elements on the innermost circumference of the solid. This is done by importing the .k file generated from ANSYS to HyperMesh and by using entity sets option.
Picked Nodes on the Innermost Surface

Picked Elements and Nodes on the Innermost Surface
Applying Pressure on the Innermost Surface
• **Case II:** To call the ConWep function, the input deck must contain *LOAD_SEGMENT* *DEFINE_CURVE* and *LOAD_BLAST* cards.

• The purpose of *LOAD_SEGMENT* is to apply pressure load over one segment defined by four nodes. Here input for LCID is −2, in order to call ConWep function.

```
*LOAD_SEGMENT
$---+-----1-----+-----2-----+-----3-----+-----4-----+-----5-----+-----6-----+-----7-----+-----8
$  LCID  SF  AT  N1  N2  N3  N4
   -2   -1.0  0   1160 1179 1180 1161
   ....
   -2   -1.0  0   2466 2485 2486 2467
   -2   -1.0  0   2467 2486 2505 2504

*LOAD_BLAST
$ WGT XBO YBO ZBO TBO IUNIT ISURF
$---+-----1-----+-----2-----+-----3-----+-----4-----+-----5-----+-----6-----+-----7-----+-----8
  0.460  0   0  0.3  0   2   2

*DEFINE_CURVE
$---+-----1-----+-----2-----+-----3-----+-----4-----+-----5-----+-----6-----+-----7-----+-----8
   4   0   1.000  1.000  0.000  0.000
  0.00000000000E+00  0.00000000000E+00
  1.00000000000E+00  0.00000000000E+00

*DEFINE_CURVE
$---+-----1-----+-----2-----+-----3-----+-----4-----+-----5-----+-----6-----+-----7-----+-----8
  25   0   1.000  1.000  0.000  0.000
  0.00000000000E+00  0.00000000000E+00
  1.00000000000E+00  0.00000000000E+00
```
The final version of .k file is then run by using LS-DYNA solver. Once the problem is successfully solved using LS-DYNA solver, the results can be viewed using either Hyper View, LS-POST, etc. Here, LS-POST was chosen.
POST-PROCESSING

- LS-DYNA is a general-purpose finite element code for analyzing the large deformation dynamic response of structures.
- LS-DYNA currently contains approximately one hundred constitutive models and ten equations-of-state to cover wide range of material behavior.
- Once the problem is successfully solved in LS-DYNA solver, the results can be viewed in many software programs like Hyper View, ANSYS, POST, etc. LS-LS-POST was chosen here.
- LS-DYNA solver outputs a d3plot output file, which is compatible with LS-POST
- Once this file is loaded, LS-POST allows viewing the nodal and elemental results.
Determination of $\epsilon_1, t_1$ and $T$ (Case I)
Determination of $\varepsilon_2$ (Case I)
Determination of $\varepsilon_3$ (Case I)
Determinations of $\frac{d\varepsilon}{dt}$ (Case I)
Determination of $\varepsilon_1$, $t_1$ and $T$ (Case II)
Determination of $\varepsilon_2$ (Case II)
Determination of $\varepsilon_3$ (Case II)
Determination of $d\varepsilon_1/d\tau$ (Case II)
## COMPARISON OF FEA AND EXPERIMENTAL RESULTS

<table>
<thead>
<tr>
<th></th>
<th>Experimental Values</th>
<th>FEA Values (Case I)</th>
<th>% Error (Case I)</th>
<th>FEA Values (Case II)</th>
<th>% Error (Case II)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Comp. Thick., $h_1^{(1)}$ [mm]</td>
<td>13.07</td>
<td>13.07</td>
<td>-</td>
<td>13.07</td>
<td>-</td>
</tr>
<tr>
<td>Outer Radius, $R_{out}^{(1)}$ [mm]</td>
<td>160.62</td>
<td>160.62</td>
<td>-</td>
<td>160.62</td>
<td>-</td>
</tr>
<tr>
<td>Steel Thick., $h_2^{(1)}$ [mm]</td>
<td>2.0</td>
<td>2.0</td>
<td>-</td>
<td>2.0</td>
<td>-</td>
</tr>
<tr>
<td>$(M1 + M2)^{(1)}$ [g]</td>
<td>23,700</td>
<td>23,700</td>
<td>-</td>
<td>23,700</td>
<td>-</td>
</tr>
<tr>
<td>$M_{HE}^{(1)}$ [g]</td>
<td>407.3</td>
<td>407.3</td>
<td>-</td>
<td>407.3</td>
<td>-</td>
</tr>
<tr>
<td>Scale factor$^{(1)}$</td>
<td>1.13</td>
<td>1.13</td>
<td>-</td>
<td>1.13</td>
<td>-</td>
</tr>
<tr>
<td>Peak Tensile Hoop Strain, $\varepsilon_1$ [%]</td>
<td>3.2</td>
<td>1.7246</td>
<td>46.10</td>
<td>1.737</td>
<td>45.72</td>
</tr>
<tr>
<td>Time to reach $\varepsilon_1$, $\tau_1$ [$\mu$s]</td>
<td>97</td>
<td>199</td>
<td>105.15</td>
<td>199</td>
<td>105.15</td>
</tr>
<tr>
<td>Peak Comp. Hoop Strain, $\varepsilon_2$ [%]</td>
<td>-0.65</td>
<td>-1.83</td>
<td>181.53</td>
<td>-1.86</td>
<td>186.15</td>
</tr>
<tr>
<td>Peak Long. Strain, $\varepsilon_3$ [%]</td>
<td>No Data</td>
<td>0.61 (-0.67)</td>
<td>-</td>
<td>0.71 (-0.75)</td>
<td>-</td>
</tr>
<tr>
<td>Period, $T$ [$\mu$s]</td>
<td>No Data</td>
<td>200</td>
<td>-</td>
<td>199.33</td>
<td>-</td>
</tr>
<tr>
<td>Max. Hoop Strain Rate, $d\varepsilon_1/dt$ [1/s]</td>
<td>524</td>
<td>565.596</td>
<td>7.93</td>
<td>495.751</td>
<td>5.39</td>
</tr>
<tr>
<td>Comments</td>
<td>Lot 2</td>
<td>Lot 2</td>
<td>-</td>
<td>Lot 2</td>
<td>-</td>
</tr>
</tbody>
</table>

Lot 2: Interchanging 13 double ring layers and 13 double spiral layers. Binder average mass fraction = 20.0%.
CONCLUSIONS AND RECOMMENDATIONS

- Open cylinder models can be used for testing the materials, which are used in nuclear reactors and containers that are used to store and/or test explosive materials.

- It has to maintain its integrity in case of accidents, else it can be fatal to the people in the vicinity as well as to the environment and hence care should be taken to ensure that these cylinders could resist blast loading.

- To validate the results obtained experimentally, finite element analysis using ANSYS and LS-DYNA was performed.

- The values of $\varepsilon_1, \varepsilon_2, t_1, \varepsilon_3, T$ and $d\varepsilon_1/dt$ obtained from LS-POST were compared with the experimental results. The difference between the experimental and FEA results was found to be good in most cases.

- However, in some cases the percentage of error was quite large and this can be attributed to the discrepancies in ConWep function and/or material properties of the composite cylinder. In addition to this, a much more finer mesh would have given better results.
REFERENCES

1. Brendan J. O’Toole, Notes obtained through email.


7. www.matweb.com